Quantum Control Theory

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December 14 (Thursday), 3:00 PM – 4:00 PM, 2023 at Prof. Stanislaw Kielich Auditorium Faculty of Physics Adam Mickiewicz University, Poznań

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Part 0. From history of control theory/engineering

• Feedback stabilization of steam engines (J. C. Maxwell "On Governors" 1868)

Feedback for robust amplifiers (H. S. Black 1927)

$$y = Tu, \ u = Fy + v \ (T \gg 1, F < 1)$$

 $\Rightarrow y = \frac{T}{1 - TF}v \approx -\frac{1}{F}v$

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(*T* Transfer function/*S*-matrix for transistor)

Part 1. QSDE and state space equation

§ Classical linear system

Hamiltonian equation

$$\frac{dX(t)}{dt} = \{H(t), X(t)\} = \frac{\partial H}{\partial p} \frac{\partial X}{\partial q} - \frac{\partial H}{\partial p} \frac{\partial X}{\partial q}$$
$$X(t) = q(t) \text{ (position) or } X(t) = p(t) \text{ (momentum)}$$
$$H(t) = \frac{m\omega^2}{2}q(t)^2 + \frac{1}{2m}p(t)^2 - q(t)u(t)$$

u(t) driving force (input)

 \Rightarrow State space equation

$$\frac{d}{dt} \begin{bmatrix} q(t) \\ p(t) \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & \frac{1}{m} \\ -m\omega^2 & 0 \end{bmatrix}}_{A} \underbrace{\begin{bmatrix} q(t) \\ p(t) \end{bmatrix}}_{x(t)} + \underbrace{\begin{bmatrix} 0 \\ 1 \end{bmatrix}}_{B} u(t)$$

$$y(t) = \underbrace{\begin{bmatrix} 1 & 0 \end{bmatrix}}_{C} \underbrace{\begin{bmatrix} q(t) \\ p(t) \end{bmatrix}}_{x(t)} (\text{output})$$

open system!

(*i.e.* feedback control based on measurement is possible.)

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§ Closed linear quantum system

CCR (Canonical Commutation Relation)

$$[\hat{q}(t), \hat{p}(t)] = \hat{q}(t)\hat{p}(t) - \hat{p}(t)\hat{q}(t) = i\hbar$$
 etc. $(i = \sqrt{-1})$

Heisenberg picture (equation)

$$\frac{d\hat{X}(t)}{dt} = \frac{i}{\hbar}[\hat{H}(t), \hat{X}(t)]$$

 \Rightarrow

$$\frac{d}{dt} \begin{bmatrix} \hat{q}(t) \\ \hat{p}(t) \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{m} \\ -m\omega^2 & 0 \end{bmatrix} \begin{bmatrix} \hat{q}(t) \\ \hat{p}(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$
(completely the same as the classical one!)
$$y(t) = ???$$
(but no output equation!)

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Only open-loop control is possible.

§ Open linear quantum system

(quantum system undergoing "continuous measurement")

 $\begin{aligned} \hat{H}(t) &= \hat{H} + \hat{H}_{c}(t) \\ \hat{H}_{c}(t) &= \chi^{T} N u(t) \quad \text{control Hamiltonian term} \\ (u(t) \quad \text{Hamiltonian modulation}) \\ (\chi &= \begin{bmatrix} \cdots & \hat{p}_{i} & \hat{q}_{i} & \cdots \end{bmatrix}^{T}) \\ \hat{L}(t) &= K \chi \quad \text{coupling operator} \\ \hat{H}(t), \hat{L}(t) \quad \text{acts on } \mathcal{H} \end{aligned}$

H(t), L(t) acts on \mathcal{H} $\hat{a}(t), \hat{a}(t)^{\dagger}$ acts on $\Gamma_{s}(\mathcal{H})$ (annihilation and creation operators on boson Fock space) $\hat{U}(t)$ acts on $\mathcal{H} \otimes \Gamma_{s}(\mathcal{H})$

Belavkin(-Hudson-Parthasarathy) QSDE (1988) (Shortly Belavkin equation)

$$d\hat{U}(t) = \left[d\hat{a}(t)^{\dagger}\hat{L}(t) - \hat{L}(t)d\hat{a}(t) - \left\{\frac{i}{\hbar}\hat{H}(t) + \frac{1}{2}\hat{L}(t)^{\dagger}\hat{L}(t)\right\}dt\right]\hat{U}(t)$$

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Heisenberg picture

$$x(t) = \hat{U}(t)^{\dagger} \chi \hat{U}(t) = \begin{bmatrix} \vdots \\ \hat{U}(t)^{\dagger} \hat{p}_{i} \hat{U}(t) \\ \hat{U}(t)^{\dagger} \hat{q}_{i} \hat{U}(t) \\ \vdots \end{bmatrix}$$

By using quantum Itô rule (H.-P. 1984) $d\hat{a}(t)d\hat{a}(t)^{\dagger} = dt$ etc. we obtain

$$dx(t) = Ax(t)dt + Bu(t)dt + B_1dw(t), \quad x(0) = x_0$$

$$dy(t) = Cx(t)dt + Du(t)dt + D_1dw(t).$$

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Part 2. Crash course for modern control theory by R. E. Kalman § State-space equation

Definition. (Continuous-time automaton) A *dynamical system* Σ is the collection (*A*, *B*, *C*, *D*) described by the *state-space equation* given below.

$$\begin{array}{rcl} \displaystyle \frac{d}{dt}x(t) &=& Ax(t) + Bu(t), \quad x(0) = x_0 \\ \displaystyle y(t) &=& Cx(t) + Du(t) \quad (t \in \mathbb{R}_{\geq 0}) \end{array}$$

$$egin{aligned} &u(t)\in\mathbb{R}^m ext{ (input), } x(t)\in\mathbb{R}^n ext{ (state),} \ &y(t)\in\mathbb{R}^p ext{ (output)} \ &A\in M_{n imes n}(\mathbb{R}), \ &B\in M_{n imes m}(\mathbb{R}), \ &C\in M_{p imes n}(\mathbb{R}), \ &D\in M_{p imes m}(\mathbb{R}) \end{aligned}$$

§ Controllability

Definition. The pair (A, B) of system Σ is *controllable* if $\forall x_0, x_1 \in \mathbb{R}^n$ and $t_1 \in \mathbb{R}_{>0}$

 $\exists (u(t))_{0 \le t \le t_1}$ such that $x(0) = x_0$ and $x(t_1) = x_1$.

Theorem. Let

$$\mathcal{C} = \begin{bmatrix} B & | & AB & | & \cdots & | & A^{n-1}B \end{bmatrix}.$$

Then the pair (A, B) is controllable \Leftrightarrow rank C = n.

Remark. C is called a controllability matrix.

§ Stabilization by state feedback

Theorem. Suppose that the pair (A, B) is controllable. Then $\exists F \in M_{n \times m}(\mathbb{R})$ such that the system $\frac{d}{dt}x(t) = (A + BF)x(t)$ with state feedback u(t) = Fx(t) is (asymptotically) stable *i.e.* $x(t) \rightarrow \vec{0}$ ($t \rightarrow \infty$) independently of $x(0) = x_0$.

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Remark.

$$\forall x(0) = x_0 \in \mathbb{R}^n \ x(t) \to \vec{0} \ (t \to \infty)$$
$$\Leftrightarrow \sigma(A + BF) \subset \{s \in \mathbb{C} \mid \operatorname{Re}(s) < 0\}$$

\S Observability.

Definition. (Observability) The pair (*A*, *C*) is *observable* if for any $t_1 > 0$ the initial condition $x(0) = x_0$ can be determined from the sequences $(u(t))_{0 \le t \le t_1}$ and $(y(t))_{0 \le t \le t_1}$.

Theorem. Let

$$\mathcal{O}^{T} = \left[\begin{array}{ccc} C^{T} & | & A^{T}C^{T} & | & \cdots & | & (A^{T})^{n-1}C^{T} \end{array} \right].$$

Then the pair (A, C) is observable \Leftrightarrow rank $\mathcal{O}^T = n$.

Remark. *O* is called an *observability matrix*.

§ (Luenberger) observer

Construction of an observer

$$\frac{d}{dt}\hat{x}(t) = A\hat{x}(t) + Bu(t) + K(\underbrace{C\hat{x}(t)}_{\hat{y}(t)} - y(t)) \quad (K \in M_{n \times p}(\mathbb{R}))$$
$$= (A + KC)\hat{x}(t) + Bu(t) - Ky(t)$$
$$\Rightarrow \frac{d}{dt}e(t) = (A + KC)e(t) \quad (e(t) = \hat{x}(t) - x(t))$$

Theorem. Suppose that (A, C) is observable. Then $\exists K \in M_{n \times p}(\mathbb{R})$ such that $e(t) \to \vec{0}$ for $t \to \infty$.

§ Stabilization by feedback $u(t) = F\hat{x}(t)$ with estimator $\hat{x}(t)$

Can u(t) = Fx(t) be replaced by $u(t) = F\hat{x}(t)$ without distabilizing the system? The entire system looks like:

$$\frac{d}{dt}x(t) = Ax(t) + Bu(t) = Ax(t) + BF\hat{x}(t)$$

$$y(t) = Cx(t)$$

$$\frac{d}{dt}\hat{x}(t) = A\hat{x}(t) + Bu(t) + K(C\hat{x}(t) - y(t))$$

$$u(t) = F\hat{x}(t).$$

Theorem. (Separation Principle) $x(t), e(t) \rightarrow \vec{0}$ for $t \rightarrow \infty$. (So the answer is YES!)

§ Transfer function

Laplace transform $X(s) = \int_0^\infty x(t)e^{-st}dt$ ($x(0) = x_0 = \vec{0}$) (similarly for $u(t) \mapsto U(s)$ and $y(t) \mapsto Y(s)$)

$$Y(s) = \underbrace{[C(sI - A)^{-1}B + D]}_{T(s)} U(s) \quad (\text{since } \frac{d}{dt} \mapsto s \cdot)$$

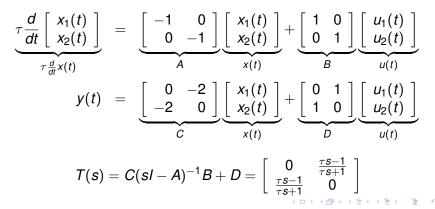
 $T(s) = C(sI - A)^{-1}B + D$ is called the *transfer function*. We say (A, B, C, D) is a *realization of* T(s).

Remark. (PAP^{-1} , PB, CP^{-1} , D) for z(t) = Px(t) is also a realization of T(s).

S T(s) as a logic gate

T(s) can be considered as a logic gate.

Example. (NOT)



If (A_i, B_i, C_i, D_i) is a realization of $T_i(s)$ (i = 1, 2) then $T_2(s)T_1(s)$ (concatenation)

and

 $T_1(s) \otimes T_2(s)$ (tensor product) are also realized using (A_i, B_i, C_i, D_i) (i = 1, 2).

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§ Linear-Quadratic Regulator (LQR)

$$\frac{d}{dt}x(t) = Ax(t) + Bu(t), \quad x(0) = x_0$$

Cost function \rightarrow minimum (*Q*, *R* positive definite matrices)

Minimization problem: $\min_{F} \int_{0}^{\infty} (x(t)^{T} Q x(t) + u(t)^{T} R u(t)) dt$

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with feedback u(t) = Fx(t) **Solution:** $F = -R^{-1}B^{T}P$ $A^{T}P + PA - PBR^{-1}B^{T}P + Q = 0$ (Riccati equation)

§ Kalman(-Bucy) filter

$$dx(t) = Ax(t)dt + Bu(t)dt + dw(t), \quad x(0) = x_0$$

$$dy(t) = Cx(t)dt + Du(t)dt + dv(t)$$

$$\mathbb{E}[w(t)w(t)^T] = Q, \quad \mathbb{E}[v(t)v(t)^T] = R \quad (\text{Gaussian})$$

Minimization problem: $\min_{\mathcal{K}} \mathbb{E}[\|\hat{x}(t) - x(t)\|^2]$

with Kalman(-Bucy) filter:

$$d\hat{x}(t) = A\hat{x}(t)dt + Bu(t)dt + K(C\hat{x}(t) - y(t))dt$$

Solution: $K = -PC^{T}R^{-1}$ $AP + PA^{T} - PC^{T}R^{-1}CP + Q = 0$ (Riccati equation) § Separarion principle for LQG=LQR+Kalman(-Bucy) filter (LQG=Linear Quadratic Gaussian)

Theorem. (Separation Principle) Replace u = Fx(t) in LQR by $u(t) = F\hat{x}(t)$ ($\hat{x}(t)$ = estimate given by Kalman filter). Then Separation Principle holds for LQR+Kalman filter.

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§ H^{∞} -control (or optimization), robust control (G. Zames)

Simple Example to give a flavor of H^{∞} -control problem

$$\frac{d}{dt}x(t) = Ax(t) + Bu(t) + w(t)$$
$$u(t) = Fx(t)$$

 $\Rightarrow X(s) = [sI - (A + BF)]^{-1}W(s)$

Replace the Gaussian assumption $w(t) \sim N(\bar{w}, Q)$ by the assumption $w(t) \in L^2(0, \infty)$.

Minimization problem: $\min_{F} \|[sI - (A + BF)]^{-1}\|_{H^{\infty}}$

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Part 3. Scattering theory and systems§ Scattering for quantum two-body problem

$$\hat{H} = -\Delta + V(x) = -\sum_{i=1}^{n} \frac{\partial^2}{\partial x_i^2} + V(x_1, \dots, x_n)$$

Schrödinger equations:

$$egin{aligned} &rac{\partial}{\partial t}|\psi(t)
angle = -rac{i}{\hbar}\hat{H}|\psi(t)
angle, \quad |\psi(0)
angle = |f
angle \ &\Rightarrow |\psi(t)
angle = e^{-rac{i}{\hbar}t\hat{H}}|f
angle = \hat{U}(t)|f
angle ext{ perturbed solution} \end{aligned}$$

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The stationary Schrödinger equation

$$(\hat{H}-k^2)|\psi
angle=0, \quad k>0$$

+ incoming and outgoing Sommerfeld radiation condition (a boundary condition at infinity)

The scattering matrix (or *S*-matrix) $S \colon L^2(\mathbb{R}_+, \mathcal{N}) \to L^2(\mathbb{R}_+, \mathcal{N})$ is defined as a mapping $\tilde{f}_{in} \mapsto \tilde{f}_{out}$:

 $\tilde{f}_{out}(k\vec{\omega}) = S(k)\tilde{f}_{in}(k\vec{\omega}) \quad (\vec{\omega} \text{ unit sphere in } \mathbb{R}^n).$

Remark. Heisenberg's scattering (or S-)matrix is

$$|f(+\infty)\rangle = S|f(-\infty)\rangle.$$

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§ Scattering model ($\{U_m(t)\}_{t \in \mathbb{R}}, \mathcal{M}$) (Continuous-time Turing machine)

$$U_m(t)$$
 acts on $\mathcal{M} = \underbrace{L^2(\mathbb{R}_-, U)}_{\text{Incoming space}} \oplus \underbrace{X}_{\text{Scattering space}} \oplus \underbrace{L^2(\mathbb{R}_+, Y)}_{\text{Outgoing space}}$

Write an element of the Hilbert space \mathcal{M} as

$$h=(u_-,x_0,y_+)\in\mathcal{M},$$

where

$$egin{aligned} u_- &= u_-(au) \in L^2(\mathbb{R}_-,U) \ (au \in \mathbb{R}_-), \quad x_0 \in X, \ y_+ &= y_+(au) \in L^2(\mathbb{R}_+,Y) \ (au \in \mathbb{R}_+). \end{aligned}$$

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The (infinitesimal) generator *L* of $\{U_m(t)\}_{t\in\mathbb{R}}$ defined by

$$Lh = \lim_{t \to 0_+} \frac{1}{t} (U_m(t)h - h), h \in \text{Dom}(L)$$

is given by $Lh = (u_1, x_1, y_1)$, where

$$\begin{array}{rcl} u_{1}(\tau) & = & -(\frac{d}{d\tau}u_{-})(\tau) & (\tau \in \mathbb{R}_{-}), \\ x_{1} & = & Ax_{0} + Bu_{-}(0), \\ y_{1}(\tau) & = & -(\frac{d}{d\tau}y_{+})(\tau) & (\tau \in \mathbb{R}_{+}), \end{array}$$

with boundary condition

$$y_+(0) = Cx_0 + Du_-(0).$$

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Transfer function and scattering matrix are related as follows.

$$T(s) = C(sI - A)^{-1}B + D = S(k) \ (s = -ik^2)$$

§ Single Electron Transistor (SET) as a scattering system



 $T(s) = C(sI - A)^{-1}B + D(=S(k))$

Feedback is given as a boundary condition

$$u_{-}(0)=Fx_{0}.$$

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